



**ERRATA**  
**to the 2021 Edition of**  
***Special Design Provisions for Wind & Seismic (SDPWS) with Commentary***

(All prior print and PDF versions)

**Page** **Revision**

13 Add the following superscript (shown in red underline) for Plywood Single Floor (under the column heading Wood Structural Panel Sheathing Type) in Table 3.2.2:

Plywood Single Floor<sup>(S)</sup>

33 Delete “s” in the following term in 4.3.5.4.1 (shown in red strike-out):

4.3.5.4.1 .... and the combined nominal unit shear capacity,  $v_{n(\text{sc})}$ , ...

91 Revise the following number in Example C4.2.6.1-2 (shown in red underline):

$\Delta_c = 0.\underline{054}$  in, joint deformation due to chord splice slip at each joint

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33     Delete the following text (shown in red strikeout) for the terms  $v_{n(1)}$  and  $v_{n(2)}$  in 4.3.5.4.1:

$v_{n(1)}$      =   nominal unit shear capacity for side 1, lbs/ft (from ~~Column A~~, Tables 4.3A, 4.3B, 4.3C, or 4.3D)

$v_{n(2)}$      =   nominal unit shear capacity for side 2, lbs/ft (from ~~Column A~~, Tables 4.3A, 4.3B, 4.3C, or 4.3D)

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41     Delete the following text (shown in red strikeout) in footnotes 1, 2, 3, 5, and 6 from Table 4.3B (footnotes 7 and 8 are not shown and remain the same):

1. Nominal unit shear capacities shall be adjusted in accordance with 4.1.4 to determine ASD allowable unit shear capacity and LRFD factored unit resistance. For general construction requirements see 4.3.6. For specific requirements, see 4.3.7.2 for wood structural panel shear walls over gypsum board. See Appendix A for common and box nail dimensions. ~~Nominal unit shear capacities are permitted to be increased to values shown for 15/32-inch (nominal) sheathing with same nailing provided (a) studs are spaced a maximum of 16 inches on center, or (b) panels are applied with long dimension across studs.~~
2. For species and grades of framing other than Douglas-Fir-Larch or Southern Pine, reduced nominal unit shear capacities shall be determined by multiplying the tabulated nominal unit shear capacity by the Specific Gravity Adjustment Factor =  $[1-(0.5-G)]$ , where G = Specific Gravity of the framing lumber from the NDS (Table 12.3.3A). The Specific Gravity Adjustment Factor shall not be greater than 1. ~~Apparent shear stiffness values,  $G_a$ , are based on nail slip in framing with moisture content less than or equal to 19% at time of fabrication and panel stiffness values for shear walls constructed with either OSB or 3-ply plywood panels. When 4-ply or 5-ply plywood panels or composite panels are used,  $G_a$  values for plywood shall be permitted to be increased by 1.2.~~
3. Apparent shear stiffness values,  $G_a$ , are based on nail slip in framing with moisture content less than or equal to 19% at time of fabrication and panel stiffness values for shear walls constructed with either OSB or 3-ply plywood panels. When 4-ply or 5-ply plywood panels or composite panels are used,  $G_a$  values for plywood shall be permitted to be increased by 1.2. ~~Where panels are applied on both faces of a shear wall and nail spacing is less than 6" on center on either side, panel joints shall be offset to fall on different framing members as shown below. Alternatively, the width of the nailed face of framing members shall be 3" nominal or greater at adjoining panel edges and nails at all panel edges shall be staggered.~~
4. Where moisture content of the framing is greater than 19% at time of fabrication,  $G_a$  values shall be multiplied by 0.5.
5. Where panels are applied on both faces of a shear wall and nail spacing is less than 6" on center on either side, panel joints shall be offset to fall on different framing members ~~as shown below~~. Alternatively, the width of the nailed face of framing members shall be 3" nominal or greater at adjoining panel edges and nails at all panel edges shall be staggered.
6. Galvanized nails shall be hot-dipped or ~~tumbled~~ mechanically deposited.



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45 Add the following text (shown in red underline) to the last sentence in 4.4.2:

The LRFD factored uplift resistance shall be determined by multiplying the tabulated nominal unit uplift capacity in Table 4.4.2 by a resistance factor,  $\phi_z$ , of 0.65.