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Revise footnote 1 in Table 12.5.1D as follows:

1. The $\ell/D$ ratio used to determine the minimum edge distance spacing between rows shall be the lesser of:
   (a) length of fastener in wood main member/D = $\ell_m/D$
   (b) total length of fastener in wood side member(s)/D = $\ell_s/D$
Claro que, pero necesito que me proporciones los datos correctos. Solo proporciono la traducción en inglés.
March 2019

ERRATA

to the 2018 Edition of

the National Design Specification® (NDS®) for Wood Construction
(all versions)

Page 167

Revised the following calculations in Example E.8 Sample Solution of Row of Split Rings
(remainder of example is unchanged):

E.8 Sample Solution of Row of Split Rings

Calculate the net section area tension and row tear-out adjusted ASD design capacities for the single-shear single-row split ring connection represented in Figure E3.

Main and Side Members:
#2 grade Southern Pine 2x4 lumber. See NDS Supplement Table 4B – Visually Graded Southern Pine Dimension Lumber for reference design values. Adjustment factors CD, CT, CM, and Ci are assumed to equal 1.0 in this example for calculation of adjusted design values.

\[
F_t' = 825\text{ psi}
\]

\[
F_v' = 175\text{ psi}
\]

Main member thickness, \(t_m\): 1.5 in.
Side member thickness, \(t_s\): 1.5 in.
Main and side member width, \(w\): 3.5 in.

Connection Details:
Split ring diameter, \(D\): 2.5 in. (see Appendix K for connector dimensions)

Adjusted ASD split ring design value, \(P'\): 2,730 lbs (see Table 13.2A. For this trial design, the group action factor, \(C_g\), is taken as 1.0).

Adjusted ASD Connection Capacity, \(nP'\):

\[
nP' = (2 \text{ split rings})(2,730\text{ lbs}) = 5,460\text{ lbs}
\]

Adjusted ASD Net Section Area Tension Capacity, \(Z_{NT}'\):

\[
Z_{NT}' = F_t'A_{\text{net}}
\]

\[
Z_{NT}' = F_t'[A_{2x4} - A_{\text{bolt-hole}} - A_{\text{split ring projected area}}]
\]

\[
Z_{NT}' = (825\text{ 675 psi})[5.25\text{ in}^2 - 1.5\text{ in} - 1.1\text{ in}^2] = 2,728\text{ 2,232 lbs}
\]

Adjusted ASD Row Tear-Out Capacity, \(Z_{RT}'\):

\[
Z_{RT}' = n_F v' A_{\text{critical}}
\]

\[
Z_{RT}' = (175\text{ psi})/(21.735\text{ in}^2) = 3,804\text{ lbs}
\]

where:

\[
A_{\text{critical}} = 21.735\text{ in}^2
\]

In this sample calculation, the adjusted ASD connection capacity is limited to \(2,728\text{ 2,232 lbs}\) by net section area tension capacity, \(Z_{NT}'\).
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<table>
<thead>
<tr>
<th>Page</th>
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<tbody>
<tr>
<td>40</td>
<td>Revise $K_{rs}$ as described in Equation (5.4-3) as follows (replace $d_e$ with $d_c$):</td>
</tr>
</tbody>
</table>

\[
K_{rs} = \text{empirical radial stress factor} = 0.29\left(\frac{d_c d_e}{R_m}\right) + 0.32 \tan^{1.2} \phi_T
\]